Coherence and Concentration in Tightly-Connected Networks

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Synchronization in Natural and Engineering Systems
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Acknowledgements



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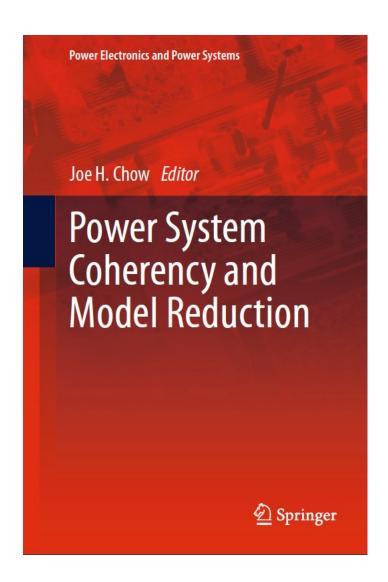




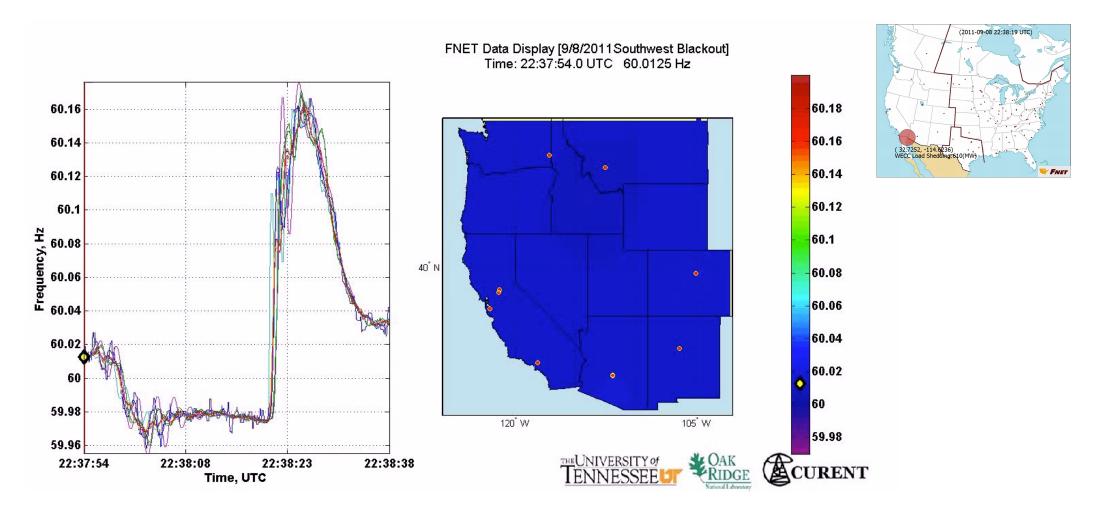


Coherence in Power Networks

- Studied since the 70s
 - Podmore, Price, Chow, Kokotovic, Verghese, Pai, Schweppe,...
- Enables aggregation/model reduction
 - Speed up transient stability analysis
- Many important questions
 - How to identify coherent modes?
 - How to accurately reduce them?
 - What is the cause?
- Many approaches
 - Timescale separations (Chow, Kokotovic,)
 - Krylov subspaces (Chaniotis, Pai '01)
 - Balanced truncation (Liu et al '09)
 - Selective Modal Analysis (Perez-Arriaga, Verghese, Schweppe '82)



This talk



Goal: Characterize the coherence response from a frequency domain perspective

Outline

- Characterization of Coherent Dynamics [Min, M '21]
- Reduced-Order Model of Coherent Response [Min, Paganini, M '21]
- Grid-forming Frequency Shaping Control [Jiang, Bernstein, Vorobev, M '21]

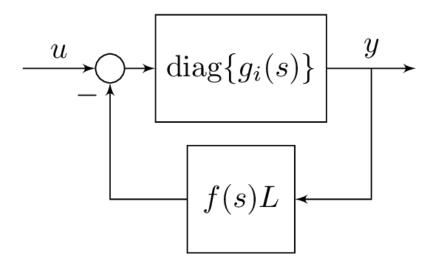
Coherence and Concentration in Tightly-Connected Networks

Hancheng Min and Enrique Mallada

ArXiv preprint: arXiv:2101.00981

Coherence in networked dynamical systems

Block Diagram:



Node dynamics: $g_i(s), i = 1, 2, \dots, n$

Symmetric Real Network Laplacian: L

$$L = V\Lambda V^T, \ V = [1/\sqrt{n}, V_{\perp}]$$

 $\Lambda = \text{diag}\{0, \lambda_2(L), \dots, \lambda_n(L)\}$

Coupling dynamics: f(s)

Examples:

Consensus Networks:

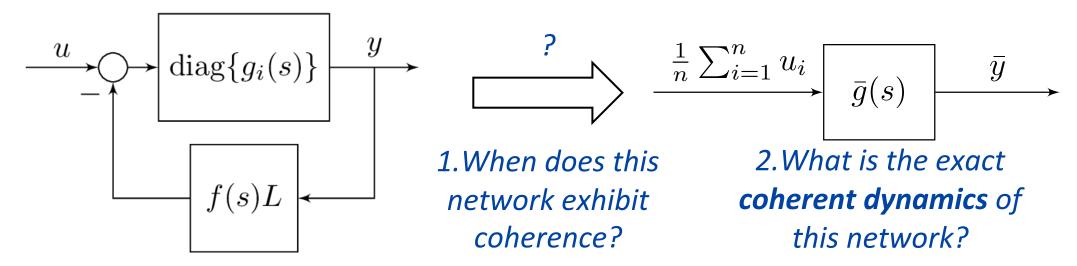
$$g_i(s) = \frac{1}{s}$$
$$f(s) = 1$$

Power Networks (2nd order generator):

$$g_i(s) = \frac{1}{m_i s + d_i + \frac{r_i^{-1}}{\tau_i s + 1}}$$
$$f(s) = \frac{1}{s}$$

Coherence in networked dynamical systems

Block Diagram:

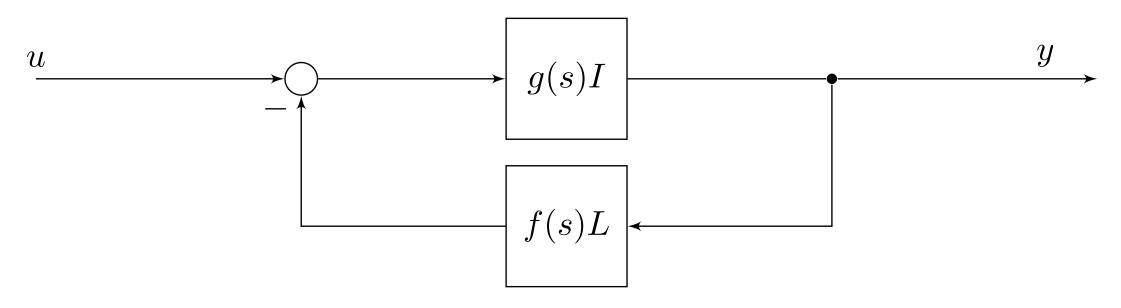


- Coherence can be understood as a low rank property the closed-loop transfer matrix
- 2. It emerges as the **effective algebraic connectivity** increases
- 3. The coherent dynamics is given by the harmonic mean of nodal dynamics

$$\bar{g}(s) = \left(\frac{1}{n} \sum_{i=1}^{n} g_i^{-1}(s)\right)^{-1}$$

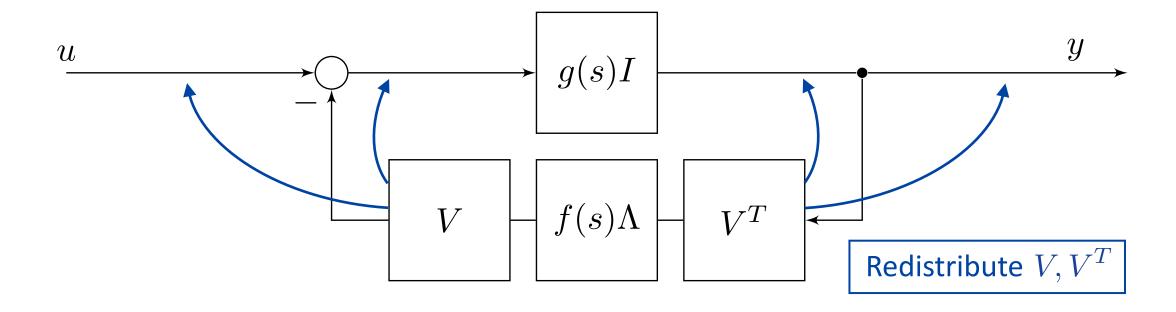
5

Assume homogeneity: $g_i(s) = g(s), i = 1, \dots, n$



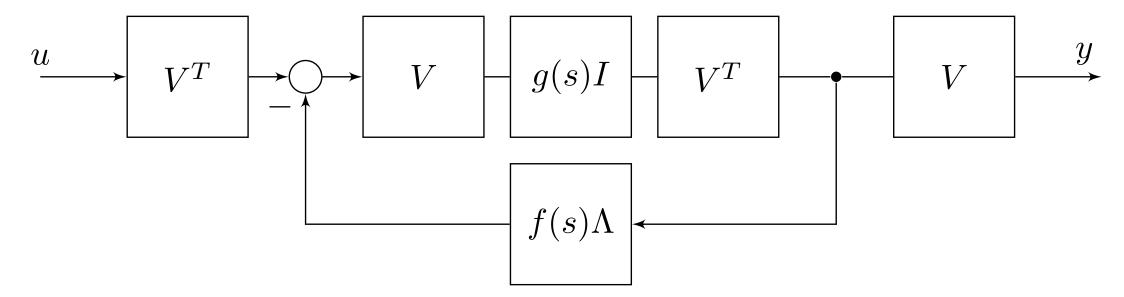
Eigendecomposition $L = V \Lambda V^T$

Assume homogeneity: $g_i(s) = g(s), i = 1, \dots, n$

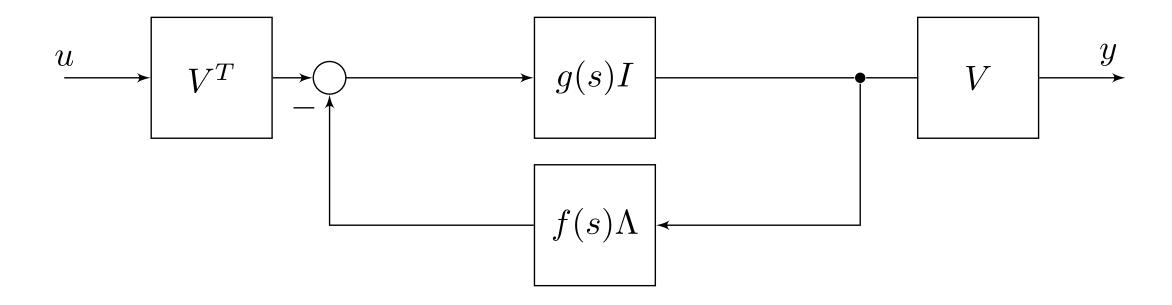


Assume homogeneity: $g_i(s) = g(s), i = 1, \dots, n$

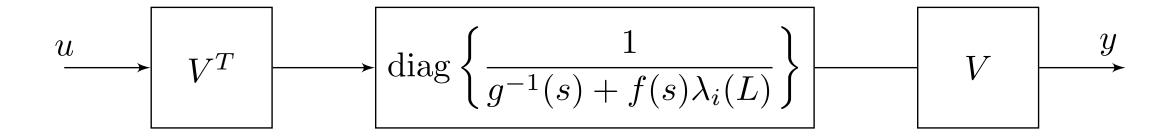
Merge forward path $\boldsymbol{V}^T\boldsymbol{V} = \boldsymbol{I}$



Assume homogeneity: $g_i(s) = g(s), i = 1, \dots, n$



Assume homogeneity: $g_i(s) = g(s), i = 1, \dots, n$



Assume homogeneity: $g_i(s) = g(s), i = 1, \dots, n$

The transfer matrix from input u to output y:

$$T(s) = V \operatorname{diag} \left\{ \frac{1}{g^{-1}(s) + f(s)\lambda_i(L)} \right\}_{i=1}^n V^T$$

$$V = [1/\sqrt{n}, V_{\perp}], \ \lambda_1(L) = 0$$

$$T(s) = \frac{1}{n}g(s)\mathbb{1}\mathbb{1}^{T} + V_{\perp}\operatorname{diag}\left\{\frac{1}{g^{-1}(s) + f(s)\lambda_{i}(L)}\right\}_{i=2}^{n} V_{\perp}^{T}$$

Coherent dynamics independent of the network structure

Dynamics dependent of the network structure

$$T(s) = \frac{1}{n}g(s)\mathbb{1}\mathbb{1}^T + V_{\perp}\operatorname{diag}\left\{\frac{1}{g^{-1}(s) + f(s)\lambda_i(L)}\right\}V^T$$

The rank-one property of the coherent dynamics leads to:

• Input aggregation, for any given input vector u(s):

$$y(s) = \frac{1}{n}g(s)\mathbb{1}\mathbb{1}^T u(s) = \frac{1}{n}g(s)\mathbb{1}\left(\sum_{i=1}^n u_i(s)\right)$$

• Output synchronization, given any two nodes i and j:

$$y_i(s) - y_j(s) = \frac{1}{n}g(s)\mathbb{1}^T u(s) - \frac{1}{n}g(s)\mathbb{1}^T u(s) = 0$$

The **rank-one** coherence dynamics effectively synchronizes the response of every node to that of $\bar{y}(s) = \frac{1}{n}g(s)\sum_{j=1}^{n}u_{j}(s)$

$$T(s) = \frac{1}{n}g(s)\mathbb{1}\mathbb{1}^T + V_{\perp}\operatorname{diag}\left\{\frac{1}{g^{-1}(s) + f(s)\lambda_i(L)}\right\}V^T$$

The effect of non-coherent dynamics vanishes as:

- The algebraic connectivity $\lambda_2(L)$ of the network increases
 - For almost any $s_0 \in \mathbb{C}$

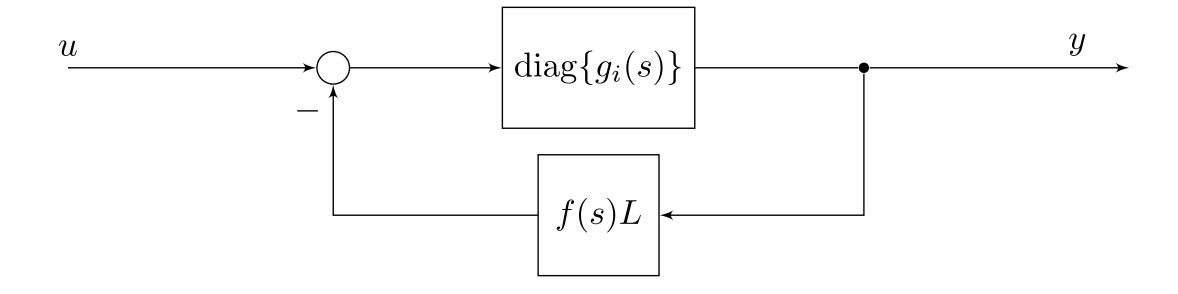
$$\lim_{\lambda_2(L) \to +\infty} \left\| T(s_0) - \frac{1}{n} g(s_0) \mathbb{1} \mathbb{1}^T \right\| = 0 \qquad \lim_{s \to s_0} \left\| T(s) - \frac{1}{n} g(s) \mathbb{1} \mathbb{1}^T \right\| = 0$$

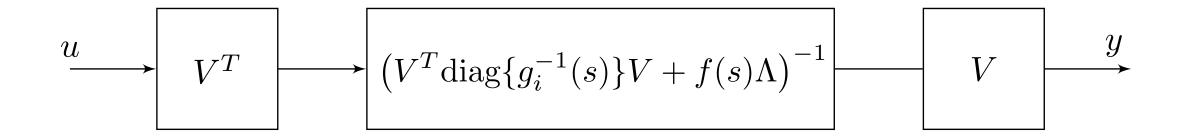
• The *s*-region of interest gets close to a **pole** of f(s)

For $s_0 \in \mathbb{C}$, a pole of f(s)

$$\lim_{s \to s_0} \left\| T(s) - \frac{1}{n} g(s) \mathbb{1} \mathbb{1}^T \right\| = 0$$

Our **frequency-dependent** coherence measure $||T(s) - \frac{1}{n}g(s)\mathbb{1}\mathbb{1}^T||$ is controlled by the **effective algebraic connectivity** $|f(s)|\lambda_2(L)$





The transfer matrix from input u to output y:

$$T(s) = V \left(V^T \operatorname{diag} \{ g_i^{-1}(s) \} V + f(s) \Lambda \right)^{-1} V^T$$

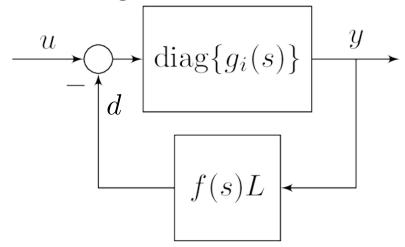
The transfer matrix from input u to output y:

$$T(s) = V \left(V^T \operatorname{diag}\{g_i^{-1}(s)\}V + f(s)\Lambda \right)^{-1} V^T$$

$$T(s) = \boxed{\frac{1}{n}\bar{g}(s)\mathbb{1}\mathbb{1}^T} + \boxed{N(s)}$$
 Coherent Network Dynamics? Dependent?

Informed guess for coherent dynamics: $\overline{g}(s)$

Block Diagram:



Coherent Dynamics:

$$\bar{y}(s) = \left(\frac{1}{n}\sum_{i=1}^n g_i^{-1}(s)\right)^{-1} \frac{1}{n}\sum_{i=1}^n u_i(s) \left| \begin{array}{c} \text{Average equations from } i=1 \text{ to } n: \\ \text{Average equations from } i$$

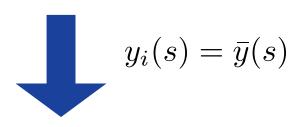
$$\bar{g}(s) = \left(\frac{1}{n} \sum_{i=1}^{n} g_i^{-1}(s)\right)^{-1}$$

Harmonic mean of all $g_i(s)$

Dynamics for node *i*

$$y_i(s) = g_i(s)(u_i(s) - d_i(s)), i = 1, \dots, n$$

Assume all nodes output are **identical** as the result of coherence



$$g_i^{-1}(s)\bar{y}(s) = u_i(s) - d_i(s), \ i = 1, \dots, n$$

$$\mathbb{1}^T L = \mathbb{0}$$

$$\left(\frac{1}{n}\sum_{i=1}^{n}g_{i}^{-1}(s)\right)\bar{y}(s) = \frac{1}{n}\sum_{i=1}^{n}u_{i}(s) - \left[\frac{1}{n}\sum_{i=1}^{n}d_{i}(s)\right]$$

$$T(s) = \frac{1}{n}\bar{g}(s)\mathbb{1}\mathbb{1}^T + T(s) - \frac{1}{n}\bar{g}(s)\mathbb{1}\mathbb{1}^T$$

$$\bar{g}(s) = \left(\frac{1}{n} \sum_{i=1}^{n} g_i^{-1}(s)\right)^{-1}$$

The effect of non-coherent dynamics vanishes as:

• For almost any $s_0 \in \mathbb{C}$

$$\lim_{\lambda_2(L) \to +\infty} \left\| T(s_0) - \frac{1}{n} \bar{g}(s_0) \mathbb{1} \mathbb{1}^T \right\| = 0 \qquad \lim_{s \to s_0} \left\| T(s) - \frac{1}{n} \bar{g}(s) \mathbb{1} \mathbb{1}^T \right\| = 0$$

• For $s_0 \in \mathbb{C}$, a pole of f(s)

$$\lim_{s \to s_0} \left\| T(s) - \frac{1}{n} \overline{g}(s) \mathbb{1} \mathbb{1}^T \right\| = 0$$

- Excluding zeros: the limit holds at zero, but by different convergence result
- We can further prove **uniform convergence** over a compact subset of complex plane, if it doesn't contain any zero nor pole of $\bar{g}(s)$
- Extensions for random network ensembles, $g_i(s) = g(s, w_i)$ (w_i random), then $\bar{g}(s) = (E_w[g^{-1}(s, w)])^{-1}$
- Convergence of transfer matrix is **related to time-domain response** by Inverse Laplace Transform

Connection to Time Domain

If $\bar{g}(s)$ and T(s) stable $(||\bar{g}||_{\infty}, ||T||_{\infty} \leq \gamma)$, then there is $\bar{\lambda} = O(\gamma/\epsilon)$ such that:

• ε -approximation, for any network L, with $\lambda_2(L) \geq \lambda$

$$\sup_{t>0} |y_i(t) - \bar{y}(t)| \le \varepsilon$$

 $\sup_{t>0}|y_i(t)-\bar{y}(t)|\leq \varepsilon$ where $\bar{y}(t)$ is the coherence dynamics response: $y(s)=\bar{g}(s)\frac{1}{n}\sum_{i=1}^n u_i(s)$

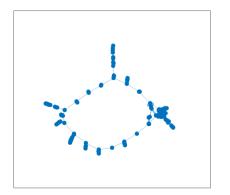
element-wise coherence, for any pair of nodes i and j

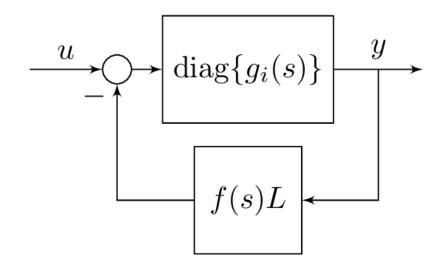
$$\sup_{t>0} |y_i(t) - y_j(t)| \le 2\varepsilon$$

Example: Icelandic Power Grid

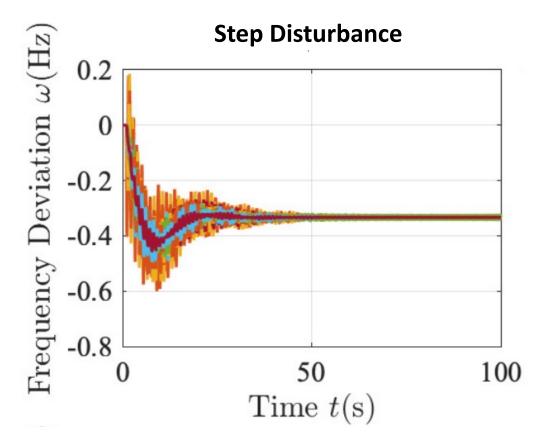
Icelandic Grid

Iceland power network: 189 buses, 35 generators, load 1.3GW (PSAT)

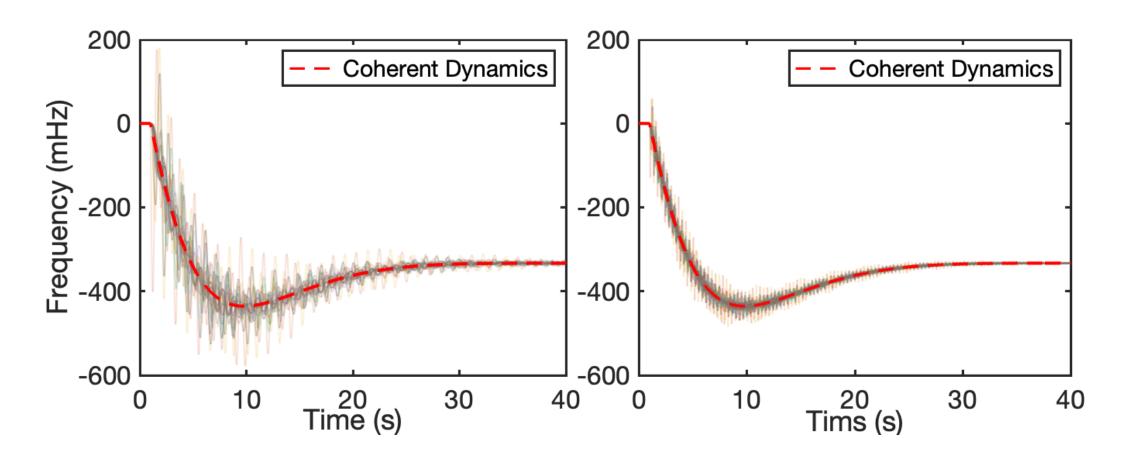




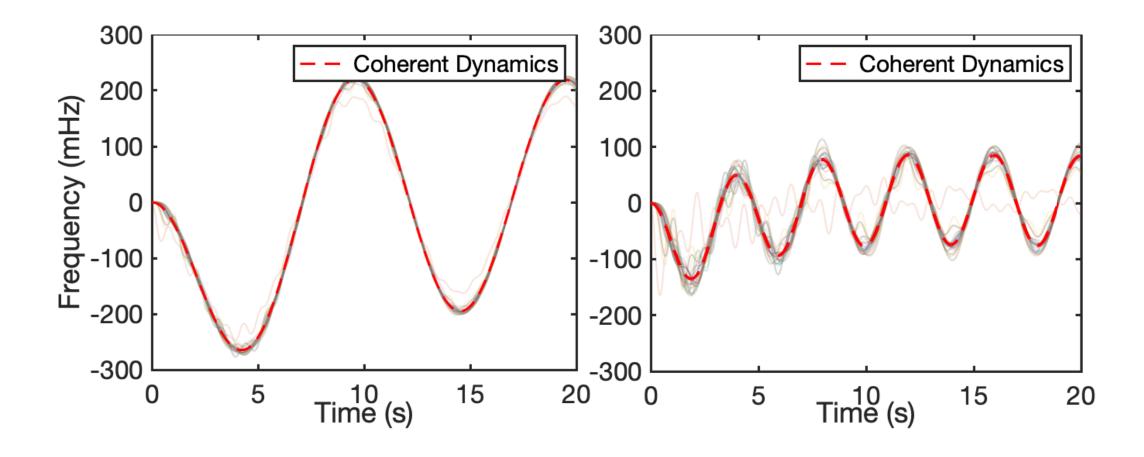
$$g_i(s) = \frac{1}{m_i s + d_i + \frac{r_i^{-1}}{\tau_i s + 1}}$$
$$f(s) = \frac{1}{s}$$



Example: Effect of Network Algebraic Connectivity $\lambda_2(L) \uparrow$



Coherent dynamics acts as a more accurate version of the Center of Inertia (CoI)



Outline

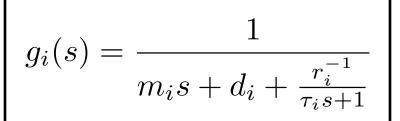
- Characterization of Coherent Dynamics [Min, M '21]
- Reduced-Order Model of Coherent Response [Min, Paganini, M '21]
- Grid-forming Frequency Shaping Control [Jiang, Bernstein, Vorobev, M '21]

Accurate Reduced-Order Models for Heterogeneous Coherent Generators

Hancheng Min, Fernando Paganini, and Enrique Mallada

IEEE Control Systems Letters, 2021

Aggregation of Coherent Generators

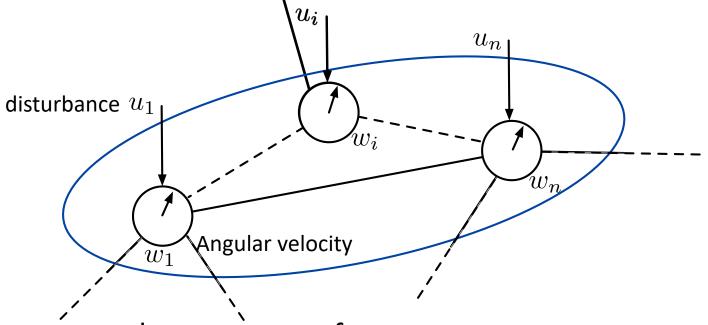


 m_i : inertia

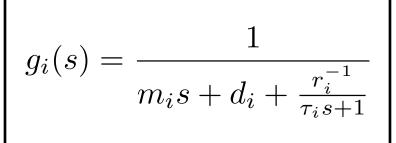
 d_i : damping coefficient

 r_i^{-1} : droop coefficient

 τ_i : turbine time constant

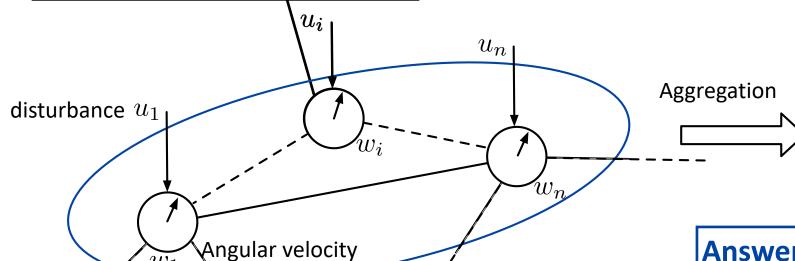


Aggregation of Coherent Generators



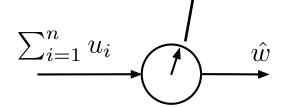
 $\widetilde{w_1}$

Question: How to choose the different parameters of $\hat{g}(s)$?



coherent group of n generators

$$\hat{g}(s) = \frac{1}{\hat{m}s + \hat{d} + \frac{\hat{r}^{-1}}{\hat{\tau}s + 1}}$$



Answer: Use instead

$$\hat{g}(s) = \frac{1}{n}\bar{g}(s) = \left(\sum_{i=1}^{n} g_i^{-1}(s)\right)^{-1}$$

Challenges on Aggregating Coherent Generators

For generator dynamics given by a swing model with turbine control:

$$g_i(s) = \frac{1}{m_i s + d_i + \frac{r_i^{-1}}{\tau_i s + 1}}$$

The aggregate dynamics:

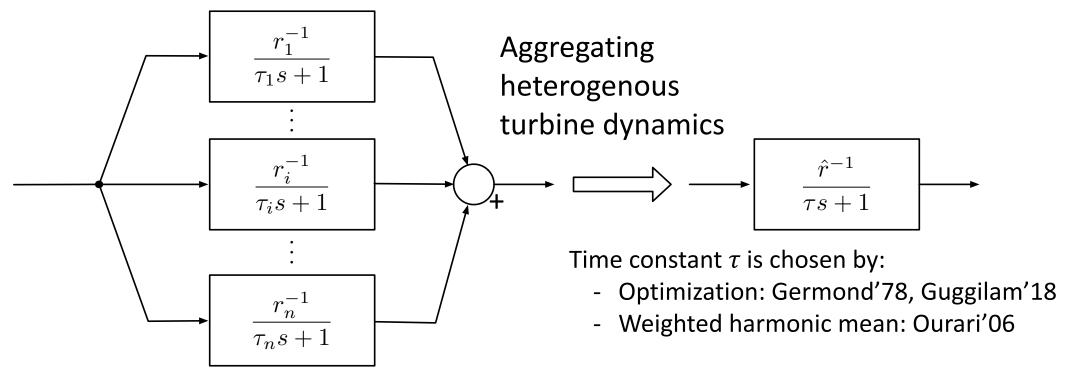
Need to find a low-order approximation of $\hat{g}(s)$

$$\hat{g}(s) = \frac{1}{\hat{m}s + \hat{d} + \sum_{i=1}^{n} \frac{r_i^{-1}}{\tau_i s + 1}}$$

high-order if τ_i are heterogeneous

Prior Work: Aggregation for heterogeneous au_i s

When time constants are **heterogenous**:



Drawbacks:

- the order of overall approximation model is restricted to 2nd order
- the only "decision variable" is the time constant
- does not consider the effect of inertia or damping in the approx.

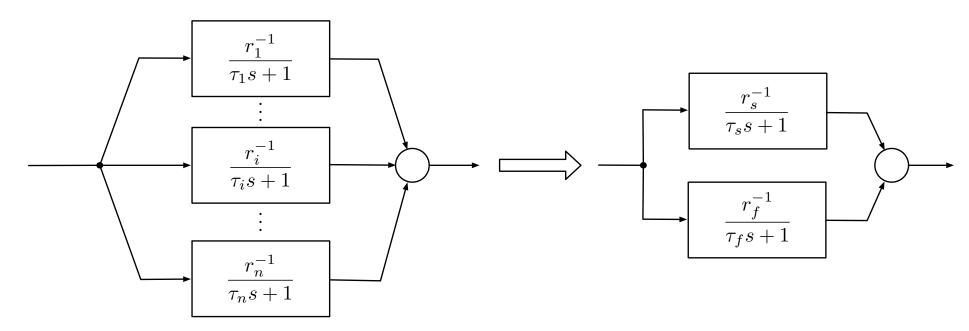
Inaccurate Approximation

Our Approach

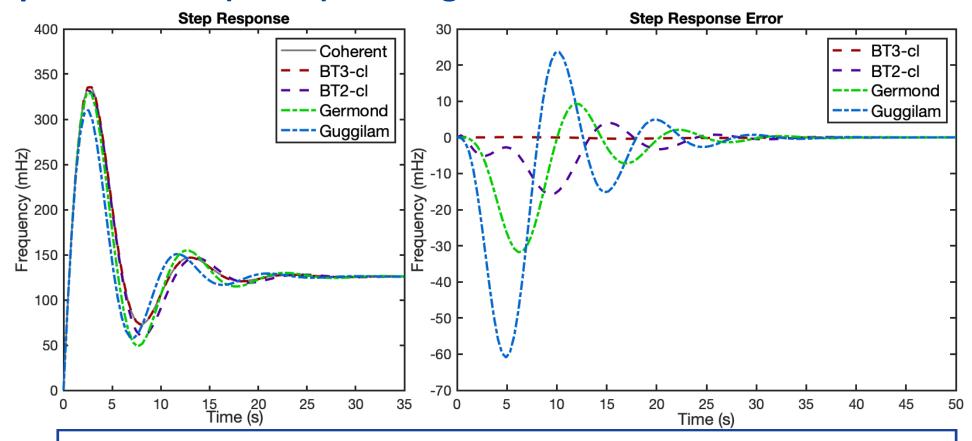
Leverage weighted balance truncation to build a hierarchy of approximations

$$\hat{g}(s) = \frac{1}{\hat{m}s + \hat{d} + \sum_{i=1}^{n} \frac{r_i^{-1}}{\tau_i s + 1}} \qquad \Longrightarrow \qquad \tilde{g}_k(s) = \frac{1}{\tilde{m}s + \tilde{d} + \tilde{g}_{tb,k-1}(s)}$$

The case k = 3, leads to a more flexible approximation



Comparison with (Some) Existing Methods



By essentially relaxing the restrictions on reduced order model:

- increase the model order to 3rd order,
- reduction on closed-loop dynamics, our proposed models outperform models by conventional approach

Outline

- Characterization of Coherent Dynamics [Min, M '21]
- Reduced-Order Model of Coherent Response [Min, Paganini, M '21]
- Grid-forming Frequency Shaping Control [Jiang, Bernstein, Vorobev, M '21]

Storage-Based Frequency Shaping Control

Yan Jiang, Eliza Cohn, Petr Vorobev, Member, IEEE, and Enrique Mallada, Senior Member, IEEE

[TPS 21]

IEEE Transactions on Power Systems, 2021

Grid-forming frequency shaping control

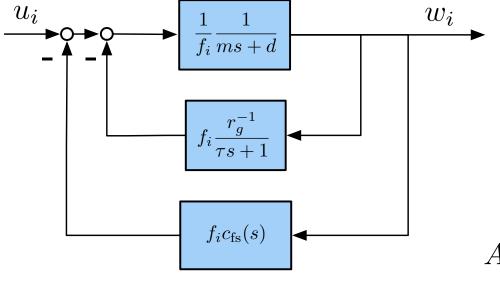
Yan Jiang¹, Andrey Bernstein², Petr Vorobev³, and Enrique Mallada¹

IEEE Control Systems Letters, 2021

[L-CSS 21]

Grid-following Frequency Shaping Control

Key idea: use model matching control (at each bus/area)



$$c_{\text{fs}}(s) := \frac{A_1 s^2 + A_2 s + A_3}{\tau s + 1}$$



$$A_1 = \tau (\mathbf{a} - m)$$

$$A_2 = \mathbf{b}\tau + \mathbf{a} - m$$

$$A_3 = \mathbf{b} - r_{g} - d$$

$$u_i$$

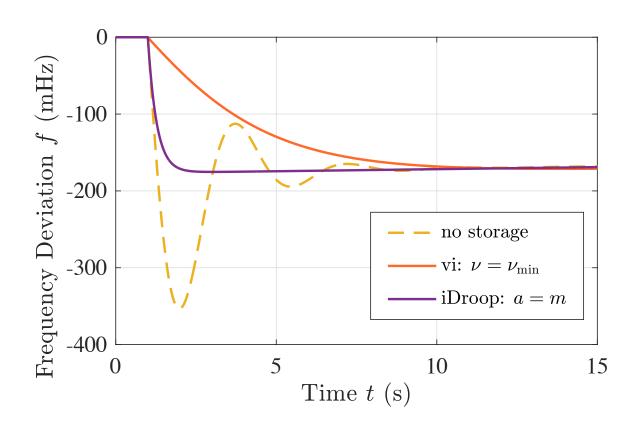
$$\frac{1}{f_i} \frac{1}{as+b}$$
 w_i

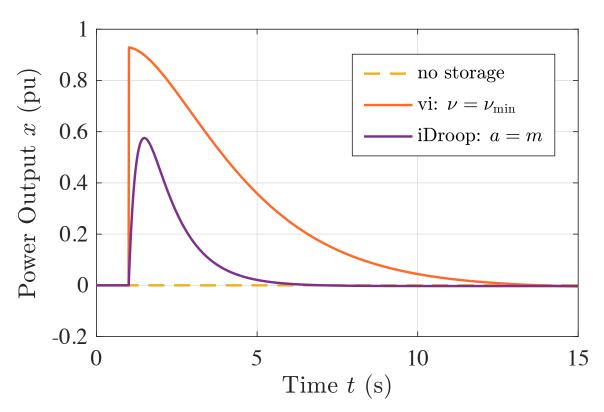
Leads to Col Frequency \overline{w} with:

RoCof:
$$||\dot{\bar{w}}||_{\infty} = \frac{|\sum_i u_{0i}|}{\sum_i f_i} \frac{1}{a}$$

Steady-state:
$$\bar{w}(\infty) = \frac{\sum_i u_{0i}}{\sum_i f_i} \frac{1}{b}$$

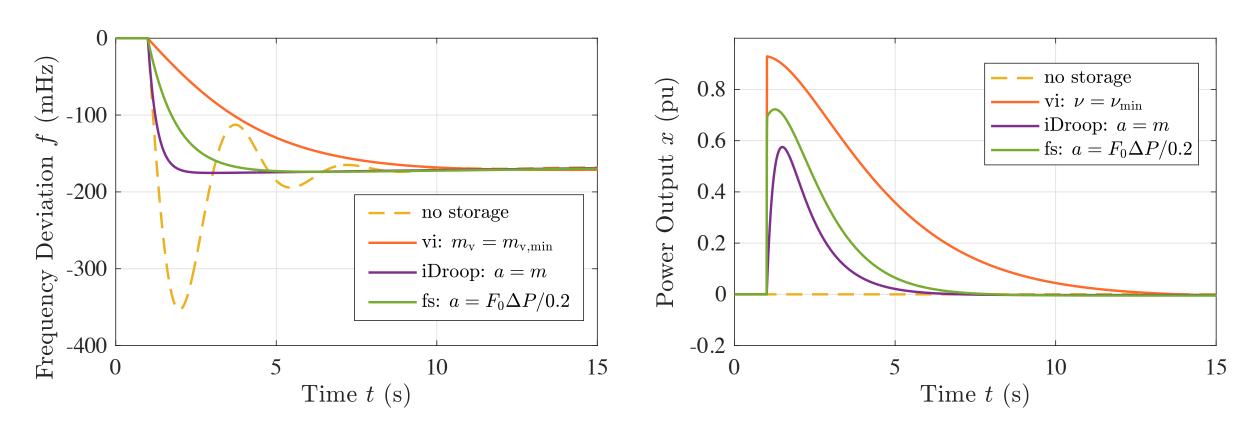
Trading off Control Effort and RoCoF





Mar 30 2022 Enrique Mallada (JHU) 16

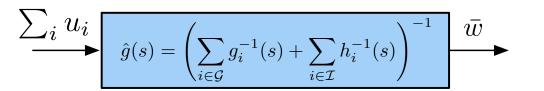
Trading off Control Effort and RoCoF



Challenge: Solution Limited to Grid-following Inverters

Grid-forming Frequency Shaping Control

Key idea: use model matching control on coherent dynamics





Generation:

$$g_i(s) = \frac{1}{m_i s + d_i + \frac{r_i^{-1}}{\tau_i s + 1}}, \quad i \in \mathcal{G}$$

$$b := \sum_{i \in \mathcal{G}} (d_i + r_i^{-1}) + \sum_{i \in \mathcal{I}} d_i$$

$$\mathbf{a} := \sum_{i \in \mathcal{G}} m_i + \sum_{i \in \mathcal{I}} m_i$$

$$b := \sum_{i \in \mathcal{G}} (d_i + r_i^{-1}) + \sum_{i \in \mathcal{I}} d_i$$

$$\sum_{i \in \mathcal{I}} c_i(s) = \sum_{i \in \mathcal{G}} \frac{r_i^{-1} \tau_i s}{\tau_i s + 1}$$

RoCoF:

$$||\dot{\bar{w}}||_{\infty} = \frac{|\sum_{i} u_{0i}|}{a}$$

Steady-state:

$$\bar{w}(\infty) = \frac{\sum_{i} u_{0i}}{b}$$

Inverters:

$$h_i(s) = \frac{1}{m_i s + d_i + c_i(s)}, \quad i \in \mathcal{I}$$

Summary

• Frequency domain characterization of **coherent dynamics**, as a low rank property of the transfer function.

- Coherence is a frequency dependent property:
 - Effective algebraic connectivity $f(s)\lambda_2(L)$
 - Disturbance frequency spectrum
- We use frequency weighted balanced truncation to suggest possible improvements to obtain accurate reduced order model of aggregated dynamics of coherent generators:
 - increase model complexity (3rd order/two turbines)
 - model reduction on closed-loop dynamics
- Grid-forming Frequency Shaping Control

Thanks!

Related Publications:

- Min, M, "Coherence and Concentration in Tightly Connected Networks," submitted
- Min, Paganini, M, "Accurate Reduced Order Models for Coherent Synchronous Generators," L-CSS 2021
- Jiang, Bernstein, Vorobev, M, "Grid-forming Frequency Shaping Control," L-CSS 2021





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Petr Vorobev Skoltech







Andrey Bernstein Fernando Paganini

Backup Slides

Numerical Examples

Modal Decomposition

Coherence